# Mixed Convection About Fruits 

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#### Abstract

Mixed convection conditions may exist when cooling field-fresh fruits. Experiments to determine convection coefficients were performed on cast models of apple, peach, plum, and strawberry shapes. Mixed convection Nusselt numbers were found to be obtainable from those for pure forced and natural convection.


## 1. Introduction

Freshly harvested fruits and vegetables are often immediately cooled to reduce spoilage. Cooling is accomplished by forcing cold fluid over them, but the combination of relatively weak forced flow and very warm objects can result in mixed forced and natural convection for fruits and vegetables. Compared to either extreme of wholly forced or natural convection, mixed convection processes are not well understood. Knowledge of mixed convection coefficients are essential for the design of heat loads for refrigeration units and for improvements in systems designed to reduce spoilage.
We have performed intensive experimental investigations on the subject of mixed convection about a sphere ${ }^{1-4}$ and have found that the heat transfer rate is a function of several factors. Among them, the forced airflow velocity (represented by the Reynolds number), the temperature difference (represented by the Grashof number), and the angle between forced airflow and natural airflow were the most important factors. The results of that research showed that there were mainly three data regions occurring with different angles: an aiding to cross flow region; a transition region; and a counter flow region. In aiding flow, forced convective flow and natural convective flow travel in the same direction. In counter flow, the two components oppose each other. In cross flow, forced air flows horizontally and natural convective air rises, forming an angle of $90^{\circ}$ between them. This study was concerned only with the cross flow case.
The Effective Diameter Scalar Addition (EDSA) method was developed to correlate experimental data for aiding and cross flows for a sphere. ${ }^{1-4}$ Using this method, mixed forced and natural convection Nusselt numbers were determined for the entire aiding flow to cross flow regime. Counter flow could be treated the same way.
The EDSA method is based upon concepts proposed by Kirk ${ }^{1}$ to describe flow patterns around the sphere and the ways in which these determine forced and natural convection heat losses. Especially interesting is the fact that the Nusselt number was found to be related to projected vertical distance of the sphere in addition to other geometrical and physical properties determining Reynolds and Grashof numbers.
The EDSA method is as follows:

1. An effective diameter ${ }^{2}$ is found from:

$$
\begin{equation*}
d_{\mathrm{eff}}=d\left[\alpha-(2 / \pi) \cos \phi \tan ^{-1}(\mathrm{Re} / \mathrm{Gr})\right] \tag{1}
\end{equation*}
$$

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## Notation

```
A,B offset in equations for irregular
        spherical object, dimensionless
        d real diameter for sphere, char-
        acteristic diameter for truit
        shaped object, m
    di diameter of largest inscribed
        circle of an irregular spherical
        object, m
    dc diameter of smallest cir-
        cumscribed circle of an irregular
        spherical object, m
    dcff effective diameter in EDSA
        method, m
    Gr Grashof number, dimensionless
    Gr* effective Grashof number in
        EDSA method, dimensionless
        g gravitational constant, }9.81\textrm{m}/\mp@subsup{\textrm{s}}{}{2
m,n coefficient in pure natural and
    forced convection equations,
        respectively, dimensionless
\(A, B\) offset in equations for irregular spherical object, dimensionless
d real diameter for sphere, characteristic diameter for fruit shaped object, m
\(d_{i}\) diameter of largest inscribed circle of an irregular spherical object, m
\(d_{c}\) diameter of smallest circumscribed circle of an irregular spherical object, m
\(d_{\text {cff }}\) effective diameter in EDSA method, m
Gr Grashof number, dimensionless
Gr* effective Grashof number in EDSA method, dimensionless \(g\) gravitational constant, \(9.81 \mathrm{~m} / \mathrm{s}^{2}\) \(m, n\) coefficient in pure natural and forced convection equations, respectively, dimensionless
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Nu Nusselt number, dimensionless
$p, q$ exponent in pure natural and forced convection equations, respectively, dimensionless
Re Reynolds number, dimensionless
Re* effective Reynolds number in EDSA method, dimensionless
$\mathrm{Re}_{\mathrm{cq}}$ equivalent Reynolds number in EDSA method, dimensionless
$t_{\text {s }} \quad$ object surface temperature, ${ }^{\circ} \mathrm{C}$
$t_{\mathrm{a}} \quad$ free stream air temperature, ${ }^{\circ} \mathrm{C}$
$\alpha$ effective diameter parameter, dimensionless
$\beta$ coefficient of thermal expansion of air, l/K
$\phi$ angle between forced and natural flow, radian
$v_{f}$ kinematic viscosity of air at mean film temperature, $\mathrm{m}^{2} / \mathrm{s}$

The value for $\alpha$ was between 0.9 and 1 in the sphere case, depending on the Grashof number. ${ }^{3,4}$ A value of 1.0 has been used in the analysis presented later in this paper.
2. An effective Grashof number then becomes:

$$
\begin{equation*}
\mathrm{Gr}^{*}=\frac{g \beta d_{\mathrm{eff}}^{3}\left(t_{\mathrm{s}}-t_{\mathrm{a}}\right)}{v_{\mathrm{f}}^{2}} \tag{2}
\end{equation*}
$$

3. The equivalent Reynolds number is a fictitious parameter that, when inserted into the forced convection Nusselt number equation, gives the correct value of Nusselt number for natural convection. The equivalent Reynolds number facilitates calculation of the mixed convection Nusselt number. To find an equivalent natural convection Reynolds number, the general empirical formula for forced convection is assumed to be: ${ }^{1-4}$

$$
\begin{equation*}
N=m \mathrm{Re}^{\mathrm{q}} \tag{3}
\end{equation*}
$$

and the general equation for natural convection was assumed to be:

$$
\begin{equation*}
N=n \mathrm{Gr}^{\mathrm{p}} \tag{4}
\end{equation*}
$$

Inserting Eqn (2) and setting Eqns (3) and (4) equal to each other to obtain an equivalent Reynolds number, we obtain:

$$
\begin{equation*}
\operatorname{Re}_{\mathrm{cq}}=\left(n / m \mathrm{Gr}^{* \mathrm{P}}\right)^{1 / \mathrm{q}} \tag{5}
\end{equation*}
$$

4. The equivalent natural convection Reynolds number is combined with the forced convection Reynolds number by scalar addition to get an effective mixed convection Reynolds number:

$$
\begin{equation*}
\mathrm{Re}^{*}=\mathrm{Re}_{\mathrm{eq}}+\mathrm{Re} \tag{6}
\end{equation*}
$$

5. Finally, a mixed convection Nusselt number is obtained using the forced convection equation:

$$
\begin{equation*}
\mathrm{Nu}=m \mathrm{Re}^{4} \tag{7}
\end{equation*}
$$

This study was intended to determine the cross flow mixed convective heat transfer coefficients for apple, peach, plum and strawberry-shaped objects, for various Reynolds and Grashof number values. This study used the EDSA method as a basis to correlate the experimental results.

## 2. Materials and methods

The experimental equipment consisted of a wind tunnel, several fruit-shaped objects, and measurement instruments. The wind tunnel was an open circuit low-speed wind tunnel designed to minimize turbulence (Fig. 1). Details of the wind tunnel, air speed measurements and temperature measurements appear in Kirk and Johnson. ${ }^{2}$ The tunnel was positioned so that horizontal forced flow and rising natural flow around the objects formed a $90^{\circ}$ angle (cross flow).

The fruit-shaped objects were modelled from an apple, a peach, a plum, and a strawberry. These objects were made of silicone rubber (GE RTV 700) compound cast from plaster moulds. This compound had a manufacturer-specified thermal conductivity of $0.23 \mathrm{~W} /(\mathrm{m} . \mathrm{K})$ compared to published thermal conductivities of $0.68 \mathrm{~W} /(\mathrm{m} . \mathrm{K})$ for strawberries and $0.42 \mathrm{~W} /(\mathrm{m} . \mathrm{K})$ for oranges. ${ }^{5}$ An electric heater made from nichrome wire wrapped around a ceramic core was placed in the centre of the object. The surfaces of the objects were first painted with a layer of conductive silver-based epoxy material in an attempt to minimize the surface temperature gradient. The surface was then coated with flat black paint to give a known surface emissivity of 0.92 .

Mohsenin ${ }^{6}$ defined the sphericity of a solid object as:

$$
\begin{equation*}
\text { Sphericity }=d_{\mathrm{i}} / d_{\mathrm{c}} \tag{8}
\end{equation*}
$$

The fruits used in this study had sphericities of $0.888,0.904,0.965$, and 0.791 , for apple, peach, plum and strawberry, respectively. From these numbers, it can be seen that the


Fig. 1. Schematic diagram of the wind tunnel used in the present experiment: (1) honeycomb section, (2) screen panels, (3) contraction zone, (4) test chamber, (5) rear honeycomb section, (6) conical reducer, (7) orifice pipe, (8) fan and motor, (9) front support assembly
peach, the plum, and the apple were nearly spherical in shape, whereas the strawberry was quite unlike a sphere.

Characteristic diameters of the objects were obtained following hydrodynamics procedures. ${ }^{7}$ First, the projected area was determined for the cross-section perpendicular to the forced airflow. Second, the projected perimeter was measured. The hydraulic radius was then obtained by dividing the projected area by the projected perimeter. The characteristic diameter was four times the hydraulic radius. ${ }^{7}$ Through this procedure, the characteristic diameters for apple, peach, plum and strawberry were determined as $0.081 \mathrm{~m}, 0.068 \mathrm{~m}, 0.057 \mathrm{~m}$ and 0.040 m , respectively.
During testing, each object was suspended in the centre of the wind tunnel test chamber. Four to six thermocouples were attached to the surface of the object, depending on its size. Each thermocouple measured a representative temperature of one of four to six segments of the surface. Meanwhile, the temperature of the testing chamber wall was measured at 11 points, each of the points represented the temperature of one of the 11 wall segments. The radiation shape factors between each surface segment and related wall segments were estimated, ${ }^{8}$ and radiation heat losses from the objects were found. Air temperature was also measured to determine air physical properties for the calculation of Reynolds number and Grashof number. Thermocouples were calibrated with a National Institute of Standards and Technology calibrated thermocouple, which has a precision of $\pm 0 \cdot 1^{\circ} \mathrm{C}$. Temperature measurement was recorded by a multichannel data acquisition system.

Air velocity was calculated from the readings of a double-sided inclined manometer used to measure the pressure drop across an orifice. Barometric pressure was measured to obtain the density of the air moving through the orifice. Measurement details were described by Kirk ${ }^{1}$ and Tang. ${ }^{3}$

Power input to the test sphere was supplied by a regulated d.c. power supply. Power was monitored as the voltage drop across the leads to the object heater and the current through a series resistor.

The experiment began with pure natural and forced convection, and then proceeded with mixed convection. The extremes of natural and forced convection were first tested so that a comparison could be made with previous results with spheres. In mixed convection, each object was tested for three different Grashof numbers. For the strawberry, the three Grashof numbers were nominally $85000 ; 120000$; and 185000 . Other objects were tested under nominal Grashof numbers of $250000 ; 500000$; and 900000 . Each group consisted of $8-12$ data points. These data points were taken on two separate days and the results showed good reproducibility.

Experimental results were obtained through the following steps.

1. The total heat loss from the object to air was obtained from the measurement of the electrical power input.
2. The radiation heat loss from the object to the testing chamber wall was calculated using measured temperatures and radiation shape factors.
3. The radiation heat loss was subtracted from the total heat loss to obtain the convection heat loss.
4. Results were grouped in the forms of dimensionless numbers.

## 3. Results

Results for pure natural convection are shown in Figs 2 and 3 and for pure forced convection in Fig. 4. Bold lines in the figures are the curves for Eqns (9) and (10). Experimental data points and curves show good agreement. Experimental results were


Fig. 2. Nusselt number versus Grashof number for natural convection. Lines through the points are calculated from Eqn (10). Data points correspond to strawberry (○), plum ( $\triangle$ ), peach (O), and apple ( $\mathbf{\Delta}$ ). The line for the sphere (centre) has no data points
compared with previous results from the study of the sphere. ${ }^{3,4}$ Fruit and sphere exhibited the same general trend, but the curves were separated by constant offsets. Because of this, the general mathematical expressions used to calculate natural and forced convection for the sphere [Eqns (3) and (4)] were modified for use with fruits. Our results could be fitted by these equations with the addition of a constant in each of them. Eqn (9) is for pure forced convection and Eqn (10) is for pure natural convection.

$$
\begin{align*}
& \mathrm{Nu}=m \mathrm{Re}^{4}+A  \tag{9}\\
& \mathrm{Nu}=n \mathrm{Gr}^{\mathrm{p}}+B \tag{10}
\end{align*}
$$

In Eqns (9) and (10), $m=0.673, n=0.336, q=0.515$, and $p=0.286$. These values were obtained from experimental observation of the sphere, ${ }^{3,4}$ described previously. Values for the factors $A$ and $B$ were determined by plotting experimental results for the fruit shapes and comparing them to the sphere. Estimated values for $A$ and $B$, which represent the differences between the sphere and the fruits, and also the differences among different fruit shapes, are shown in Table 1. Although the curve for the strawberry does not appear to be parallel to that of the sphere in Fig. 2, it can be seen from Fig. 3 that the two curves are indeed parallel.
Differences in Nusselt number between the regular-shaped and smooth-surfaced sphere and the irregularly shaped and rougher-surfaced fruit models can be shown by considering the plum. The plum model is about the same size ( 0.057 m characteristic diameter) as the sphere ( 0.0575 m diameter), but the plum has a higher Nusselt number for both forced


Fig. 3. Nusselt number versus Grashof number for natural convection from the strawberry. Although the strawberry line () does not appear to be parallel to the sphere line (without points) in Fig. 2, it clearly appears parallel when replotted on this expanded scale
and natural convection. This was probably due to the irregularity of the plum shape, which probably caused more turbulence and vortices along the surface. ${ }^{9}$

Among the fruit models, the larger-sized fruit exhibited smaller Nusselt numbers for both natural and forced convection. Typical surface temperature distributions in Tables 2 and 3 are the likely reasons for this.

The surface of the plum was divided into four segments (top windward, bottom windward, top leeward and bottom leeward) and surface thermocouples were attached to each segment. In the natural convection case, the temperature showed a tendency to be higher in the top segments and lower in the bottom segments. This indicates that the rising hot air accumulated around the top part of the model, which caused a smaller temperature difference between the air and surface (which is the driving force of natural convection( around the top part of the model. This resulted in lower natural convection from the top, and surface temperatures of that part increased. Comparing Tables 2 and 3 , it can be seen that at nearly the same Grashof number, the peach had a larger temperature difference between the bottom and the top. Thus, the larger peach had a lower convection coefficient than the smaller plum.

In the case of forced flow, Tables 2 and 3 show that there was a significant temperature difference between the windward and leeward sides of the surface. This indicates that there was much smaller forced flow on the leeward side. This conclusion has also been shown by smoke flow patterns by Tang. ${ }^{3,9}$ The larger object with the smaller surface


Fig. 4. Nusselt number versus Reynolds number for forced convection. Lines through the points are calculated from Eqn (9). Data points correspond to strawberry $(\bigcirc)$, plum $(\triangle)$, peach $(\bigcirc)$, and apple $(\mathbf{\Delta})$. The line for the sphere is in the centre

Table 1
$A$ and $B$ values for different fruits

|  | Apple | Peach | Plum | Strawberry |
| :---: | :---: | :---: | :---: | :---: |
| $A$ | -4 | -2 | 1 | 5 |
| $B$ | -2 | -1 | 1 | 3.5 |

Table 2
Typical surface temperature ( ${ }^{\circ} \mathrm{C}$ ) distribution for plum

|  | Top <br> windward | Bottom <br> windward | Top <br> leeward | Bottom <br> leeward |
| :--- | :---: | :---: | :---: | :---: |
| Natural | 41.2 | 38.2 |  | 40.9 |
| Forced | 37.6 | 36.5 | 42.6 | 38.7 |

Natural convection data is at a Grashof number of 305500.

Forced convection data is at a Grashof number of 385 200, and a Reynolds number of 6539.

Windward and leeward terms refer to forced flow.

Table 3

|  | Top windward | Bottom windward | Top leeward | Bottom leeward |
| :---: | :---: | :---: | :---: | :---: |
| Natural | 41.4 | $35 \cdot 4$ | 41.5 | $34 \cdot 1$ |
| Forced | 29.0 | $28 \cdot 2$ | $34 \cdot 2$ | $32 \cdot 3$ |

Natural convection data is at a Grashof number of 347900.

Forced convection data is at a Grashof number of 310100 , and a Reynolds number of 5526.


Fig. 5. Nusselt number versus actual Reynolds number for mixed convection at a Grashof number of 250000. Lines through the points are calculated using methods described in the text. Data points correspond to plum ( $(\square)$, peach $(\bigcirc)$, and apple $(\triangle)$
curvature blocked the leeward air flow more completely, leaving a larger portion of the leeward side untouched by the forced airflow. Thus the overall Nusselt number decreased.
Mixed convection Nusselt numbers were found to be calculable using the EDSA method as described previously. Since Eqns (3) and (4) were changed to Eqns (9) and (10), Eqn (5) now takes the form of:

$$
\begin{equation*}
\mathrm{Re}_{\mathrm{cq}}=\left[\left(n \mathrm{Gr}^{* \mathrm{p}}-A+B\right) / \mathrm{m}\right]^{1 / \mathrm{q}} \tag{11}
\end{equation*}
$$

With thesc modifications, the procedure for the EDSA method was found to give accurate results.

Fig. 5 shows some typical mixed convection curves for plum, peach and apple. Curves were obtained using the EDSA method with values of $A$ and $B$ appearing in Table 1. Points are actual measured data.

Since the characteristic diameter of the strawberry was significantly smaller than all the other objects, its Grashof number testing range was much lower than others, and its results could not be put onto the same graph with the others. However, even with Grashof number values between 85000 and 180000 , which is much smaller than the Grashof values of 250000 to 900000 for the other objects, the Nusselt numbers for the strawberry are equal to or higher than those of the others. Fig. 6 shows the mixed convection curves for the strawberry. Recall from the equipment section that the


Fig. 6. Nusselt number versus actual Reynolds number for mixed convection for the strawberry. Lines through the points are calculated using methods described in the text. Data points correspond to Grashof number values of $85000(\triangle), 110000(\bigcirc)$, and 180000 ( $\square$ ).
strawberry used in this experiment had the most irregular shape. This irregularity probably caused more turbulence and vortices, which then caused stronger heat transfer.

## 4. Discussion

We have provided not only convection data for several fruit shapes in wholly forced and natural flows, but also a means to combine the two to predict mixed convection. From this standpoint, this experiment and analysis of experimental results were successful.

However, several questions still remain. Surface temperature differences of several degrees were measured on our models (in some larger models, it even exceeded $10^{\circ} \mathrm{C}$ ). What are the implications if this is the same for real fruit? These hot spots could be more subject to local spoilage than cooler spots. Also, higher Nusselt numbers were attributed to shape irregularities compared to the sphere. Are there other major factors that also influence the heat transfer rate?

Characterizing the sizes of these models caused great difficulty. Certainly, irregularity of shape was not easy to deal with. Orientation of the fruit with respect to the direction of airflow may significantly change the results.

Values for the constants $A$ and $B$ were determined by eye rather than by some other means. Perhaps those who would wish to use these values would like to make more precise estimates, and they may from data in the Appendix and from the equations for forced and natural convection from a sphere. However, added precision in the estimates for $A$ and $B$ does not guarantee added accuracy for future calculations. It is just as important that we know that equations for the sphere can be modified for fruits by adding or subtracting constant values as it is to know values of the constants. Given the variability of fruit shapes, our values for $A$ and $B$ are about as precise as they need to be.

It is interesting to speculate about a parallel between equations for convection from a sphere and those determined in this paper to apply to fruit. The equation to correlate spherical convection data is often given as: ${ }^{10}$

$$
\begin{equation*}
N=2 \cdot 0+m \operatorname{Re}^{4} \tag{12}
\end{equation*}
$$

where the constant term is used to account for convection in totally still environments. Actually, heat is transferred by conduction in totally still environments, so the constant term does not appear where natural convection could arise.

Constants determined in this paper for the various fruits are not likely to have the same meaning as the 2.0 in Eqn (12). Our models were heated and so were free to develop natural convection instead of conduction. More likely, the constants in our equations are the result of vortex shedding and turbulence. If this is the case, one would not expect the distances between natural and forced convection curves to be constant as the condition of still air is approached.

Using a moulding compound with lower thermal conductivity than appears in real fruit would have had some affect on the experimental results, but exactly how much is not clear. Since convection is a surface phenomenon, and the shape of the fruit models is the same as the fruits themselves, measured convection coefficients should be basically correct, but with an indirect influence of the moulding compound. The lower thermal conductivity probably contributed to surface temperature non-uniformity, and this would influence overall convection coefficients. Nevertheless, the moulding compound thermal conductivity differs from the expected fruit thermal conductivity by only a factor of 2-3 and not by orders of magnitude. Therefore, some temperature non-uniformity would be expected to appear on the surface of real fruits, and convection coefficients for the fruits are probably not too different from those measured for the models.

The last item for discussion is the relation of this experiment and its results to practical situations. Fruit is not usually cooled singly and separated from other fruit. Thus, of what practical importance are the results from this experiment?

Our approach to the problem of mixed convection has been systematic: we first tested spheres with the idea that mixed convection Nusselt numbers should be determinable from equations related to pure forced and pure natural convection. The EDSA approach resulted from those experiments, and the importance of the EDSA method is that mixed convection Nusselt number can be determined for any combination of Reynolds and Grashof numbers without experiments designed to test specific combinations.

Results in this paper demonstrate the correctness of our approach. Without the experience with the sphere to draw from, a systematic approach to mixed convection Nusselt number from fruit-shaped objects would have been much more difficult to achieve. By comparing the fruits with the sphere, analogies become apparent, and we found that the EDSA method, slightly modified from the sphere, could work with fruits. Although there are fruit shapes we did not test, we can deduce that the forms of the pure natural and pure forced convection equations, and their combinations to mixed convection, will likely be similar to those determined in this experiment, with differences in the values of $A$ and $B$ to distinguish other shapes.

It does not take much imagination to realize that the next step in this process is to test packed fruits to see if mixed convection can be determined from pure forced and pure natural convection relationships. Therefore, the practical use of this experiment is the idea that results from ideal shapes can be extended to cover non-ideal shapes. Packed fruit represents another step away from the ideal.

## 5. Conclusions

Mixed convective Nusselt numbers for isolated fruit shapes can be predicted from convection equations for pure forced and natural convection. These equations are the same as those for a sphere with the addition of constant numbers.

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## Appendix

Natural, forced, and mixed convection experimental data are difficult to obtain and are therefore rarely found. Since these data may be valuable for some readers, they are included in this appendix.

Table A1

| Natural convection data |  |  |  |
| :---: | :---: | :---: | :---: |
| Fruit | Grashof number | Nusselt number |  |
|  |  | Observed | Predicted |
| Strawberry | 20010 | $10 \cdot 3$ | 9.31 |
|  | 75050 | $11 \cdot 3$ | 11.8 |
|  | 105040 | $13 \cdot 1$ | 12.7 |
|  | 145100 | $13 \cdot 2$ | $13 \cdot 6$ |
|  | 205000 | 14.3 | 14.6 |
|  | 251030 | 15.7 | $15 \cdot 3$ |
|  | 325100 | 16.8 | $16 \cdot 2$ |
| Plum | 291000 | $13 \cdot 3$ | $13 \cdot 3$ |
|  | 259000 | $14 \cdot 3$ | $14 \cdot 0$ |
|  | 487000 | $15 \cdot 5$ | $15 \cdot 2$ |
|  | 598000 | $16 \cdot 2$ | $16 \cdot 1$ |
|  | 695000 | $16 \cdot 5$ | $16 \cdot 7$ |
|  | 841000 | $17 \cdot 3$ | 17.6 |
|  | 1033000 | 18.0 | 18.6 |
| Peach | 368000 | 11.8 | $12 \cdot 1$ |
|  | 477000 | 12.8 | $13 \cdot 1$ |
|  | 598000 | $13 \cdot 8$ | $14 \cdot 1$ |
|  | 704000 | 14.8 | 14.8 |
|  | 805000 | $15 \cdot 4$ | 15.4 |
|  | 947000 | 16.4 | 16.2 |
|  | 1072000 | $16 \cdot 9$ | 16.8 |
|  | 1251000 | 17.9 | 17.6 |
| Apple | 151000 | 8.58 | 8.17 |
|  | 198000 | 9.63 | 8.99 |
|  | 348000 | 9.95 | 10.9 |
|  | 541000 | 12.7 | $12 \cdot 7$ |
|  | 743000 | 14.2 | 14.0 |
|  | 939000 | $14 \cdot 8$ | $15 \cdot 2$ |
|  | 1173000 | 15.9 | $16 \cdot 3$ |
|  | 1633000 | 17.0 | 18.1 |

Predicted Nusselt number is $0.336 \mathrm{Gr}^{1 \cdot 2 \times 6}+B$, where $B=-2,-1,1$, and $3 \cdot 5$ for apple, peach, plum, and strawberry shapes.

Table A2
Forced convection data

| Fruit | Reynolds number | Nusselt Observed | number Predicted |
| :---: | :---: | :---: | :---: |
| Strawberry | 1411 | 30.9 | 33.2 |
|  | 1782 | $35 \cdot 1$ | $36 \cdot 8$ |
|  | 2310 | $40 \cdot 2$ | $41 \cdot 3$ |
|  | 2825 | $45 \cdot 4$ | $45 \cdot 3$ |
|  | 3756 | 48.9 | 51.7 |
|  | 4011 | 53.9 | $53 \cdot 3$ |
|  | 4517 | 57.8 | 56.3 |
| Plum | 2028 | 32.9 | $35 \cdot 0$ |
|  | 2477 | $36 \cdot 9$ | $38 \cdot 7$ |
|  | 3032 | 41.0 | 42.8 |
|  | 3610 | $46 \cdot 1$ | $46 \cdot 7$ |
|  | 4287 | 50.0 | 51.0 |
|  | 4330 | $53 \cdot 6$ | $51 \cdot 2$ |
|  | 5291 | 57.2 | $56 \cdot 7$ |
|  | 6316 | $63 \cdot 8$ | $62 \cdot 0$ |
| Peach | 3232 | 42-1 | 41.2 |
|  | 3794 | $44 \cdot 8$ | 44.9 |
|  | 4402 | 47.9 | $48 \cdot 6$ |
|  | 5032 | 52.4 | $52 \cdot 3$ |
|  | 5738 | 54.5 | $56 \cdot 0$ |
|  | 6845 | 59.4 | 61.6 |
|  | 7668 | 63.8 | 65.4 |
|  | 8254 | $66 \cdot 1$ | $68 \cdot 0$ |
| Apple | 4641 | 48.0 | 48.0 |
|  | 5398 | $50 \cdot 5$ | 52.2 |
|  | 6113 | 55.0 | $56 \cdot 0$ |
|  | 7065 | $58 \cdot 0$ | $60 \cdot 6$ |
|  | 7789 | 61.7 | 63.9 |
|  | 8471 | 64.5 | $66 \cdot 9$ |
|  | 9322 | $67 \cdot 0$ | $70 \cdot 5$ |
|  | 9661 | $71 \cdot 2$ | 71.9 |
|  | 10284 | $76 \cdot 1$ | 74.4 |

Predicted Nusselt number is $0.673 \mathrm{Re}^{0.515}+A$, where $A=-4,-21$, and 5 , for apple, peach, plum, and strawberry shapes.

Table A3
Mixed convection data

| Fruit | Reynolds number | Grashof number | Nusselt number observed |
| :---: | :---: | :---: | :---: |
| Apple | 563 | 251000 | 15.35 |
|  | 578 | 252000 | $15 \cdot 56$ |
|  | 624 | 249000 | 15.98 |
|  | 660 | 250000 | $15 \cdot 34$ |
|  | 689 | 251000 | 16.23 |
|  | 723 | 247000 | 16.78 |
|  | 743 | 248000 | 17.06 |
|  | 821 | 249000 | 17.64 |
|  | 828 | 250000 | 18.45 |
|  | 905 | 251000 | 18.67 |
|  | 930 | 252000 | 18.89 |
|  | 983 | 249000 | 19.45 |
|  | 1015 | 250000 | 20.45 |
|  | 1173 | 251000 | 22.63 |
|  | 245 | 514000 | 15.67 |
|  | 283 | 507000 | 15.81 |
|  | 335 | 502300 | $16 \cdot 34$ |
|  | 381 | 512000 | 16.58 |
|  | 430 | 523000 | 16.99 |
|  | 485 | 513000 | 17.01 |
|  | 535 | 508000 | 17.34 |
|  | 595 | 511000 | 17.88 |
|  | 659 | 515000 | $18 \cdot 12$ |
|  | 704 | 507000 | $18 \cdot 19$ |
|  | 243 | 912000 | 17.89 |
|  | 293 | 910000 | 18.75 |
|  | 348 | 909000 | 18.54 |
|  | 391 | 908000 | 18.77 |
|  | 442 | 909000 | 19.43 |
|  | 489 | 907000 | 19.52 |
|  | 545 | 912000 | 19.88 |
|  | 595 | 911000 | 20.25 |
|  | 644 | 910000 | 20.43 |
|  | 702 | 909000 | 20.64 |
| Peach | 485 | 251000 | 16.26 |
|  | 565 | 250000 | 17.14 |
|  | 575 | 247000 | 17.54 |
|  | 624 | 249000 | 17.95 |
|  | 663 | 250000 | $18 \cdot 10$ |
|  | 692 | 251000 | 18.23 |
|  | 725 | 249000 | 18.43 |
|  | 747 | 248000 | 18.73 |
|  | 817 | 250000 | 18.95 |
|  | 830 | 254000 | 19.43 |
|  | 903 | 252000 | 20.07 |
|  | 934 | 250000 | 20.74 |
|  | 983 | 251000 | 21.05 |
|  | 263 | 513000 | 16.99 |
|  | 279 | 509000 | 17.13 |
|  | 323 | 515000 | 17.53 |
|  | 376 | 512000 | 17.70 |
|  | 423 | 510000 | 17.88 |
|  | 488 | 508000 | 18.24 |
|  | 532 | 509000 | 18.47 |
|  | 586 | 511000 | 19.10 |
|  | 634 | 512000 | 19.56 |
|  | 240 | 905000 | 19.53 |
|  | 288 | 904000 | 19.67 |
|  | 331 | 906000 | 19.94 |

Table A3-(Contd.)

| Fruit | Reynolds number | Grashof number | Nusselt number observed |
| :---: | :---: | :---: | :---: |
| Peach | 382 | 904000 | 20.44 |
|  | 423 | 903000 | 20.67 |
|  | 479 | 902000 | 20.54 |
|  | 523 | 903000 | 20.69 |
|  | 583 | 904000 | 20.97 |
|  | 635 | 903000 | 21.35 |
|  | 688 | 904000 | $21 \cdot 66$ |
| Plum | 420 | 254000 | 16.79 |
|  | 484 | 249000 | 17.34 |
|  | 565 | 250000 | $18 \cdot 35$ |
|  | 580 | 251000 | 18.88 |
|  | 628 | 251000 | 19.57 |
|  | 665 | 250000 | 19.95 |
|  | 691 | 249000 | $20 \cdot 13$ |
|  | 728 | 248000 | 20.85 |
|  | 745 | 250000 | 21.04 |
|  | 819 | 249000 | 21.24 |
|  | 831 | 250000 | 22.05 |
|  | 240 | 507000 | 19.03 |
|  | 285 | 508000 | 19.34 |
|  | 325 | 509000 | 19.61 |
|  | 375 | 509000 | $20 \cdot 14$ |
|  | 419 | 515000 | $20 \cdot 54$ |
|  | 478 | 503000 | 20.88 |
|  | 522 | 504000 | 21.09 |
|  | 576 | 505000 | $21 \cdot 23$ |
|  | 637 | 504000 | 21.76 |
|  | 688 | 505000 | 21.93 |
|  | 245 | 893000 | $20 \cdot 34$ |
|  | 289 | 901000 | 20.89 |
|  | 334 | 900000 | $21 \cdot 13$ |
|  | 389 | 898000 | 21.99 |
|  | 445 | 903000 | 22.67 |
|  | 499 | 904000 | 23.06 |
|  | 542 | 898000 | 23.54 |
|  | 599 | 902000 | 24.01 |
|  | 654 | 901000 | 24.43 |
| Strawberry | 275 | 83400 | $17 \cdot 18$ |
|  | 315 | 83800 | 17.68 |
|  | 363 | 84300 | 18.01 |
|  | 425 | 84800 | 18.85 |
|  | 480 | 85100 | 19.62 |
|  | 520 | 85200 | 20.84 |
|  | 560 | 85500 | 21.55 |
|  | 277 | 107000 | 17.65 |
|  | 318 | 108000 | 17.93 |
|  | 362 | 110000 | 18.69 |
|  | 427 | 111000 | 19.74 |
|  | 483 | 109000 | $20 \cdot 32$ |
|  | 523 | 108000 | 21.60 |
|  | 562 | 110000 | 22.47 |
|  | 273 | 176000 | 18.48 |
|  | 312 | 178000 | 19.07 |
|  | 361 | 181000 | $19 \cdot 54$ |
|  | 423 | 180000 | 20.56 |
|  | 478 | 182000 | 21.56 |
|  | 517 | 179000 | 22.35 |
|  | 558 | 180000 | 22.93 |

